

## Non-isolated switching regulators Application Guide 2017

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## I. Selection Guide

The steps are shown as follows.

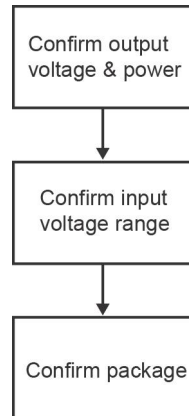


Diagram 1-1 Steps of selecting switching regulators

### First, confirm output voltage and power.

Output voltage and power come first when selecting a power supply. Non-isolated switching regulators have a full range of output voltages: 1.2V, 1.5V, 1.8V, 2.5V, 3.3V, 5V, 6.5V, 9V, 12V, 15V and 24V.

Regarding output power, the regulators are suffixed with output currents such as 500mA and 1000mA. At present, available output currents are 500mA, 1000mA, 1500mA and 2000mA.

Output current can be determined once the load is confirmed. The load current determines power and affects the converter's reliability and price. It is suggested that the converter is used in a load range of 30%-80% of its output power at ambient temperature. Choosing the correct output current is one of the key factors in successful design, incorrect selection may lead to lower reliability. Given that the converter has to be used at high temperature of over 70 °C for a long time, please contact our sales department for more information.

### Second, confirm input voltage range.

MORNSUN non-isolated switching regulators use a step-down circuit design, the input voltage should be at least 3V greater than the output voltage. Common input ranges

are 4.75-28V, 6.5-32V, 4.75-18V and 9-72V.

### Third, confirm package.

The regulators are mainly in DIP, SIP and SMD package, the first two types can be supplied with bent input pins for horizontal mount. In either form they are compatible with LM78XX linear regulators in TO-220 packages.

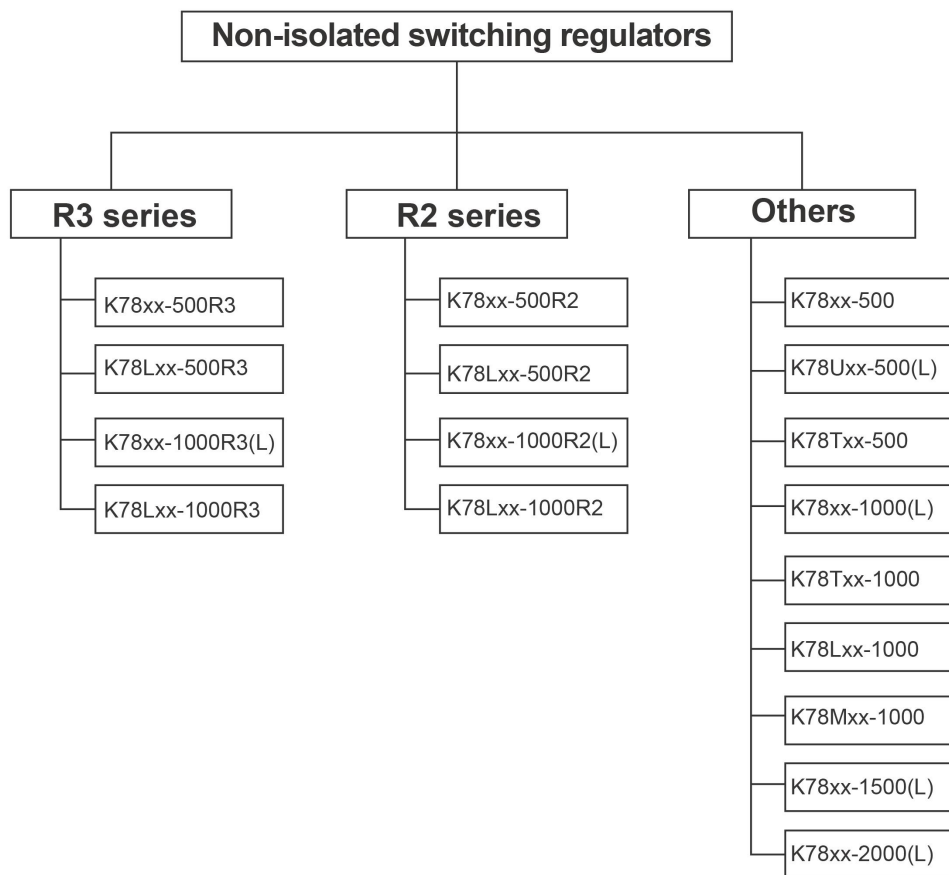


Diagram 1-2 Selection Block Diagram

For example:

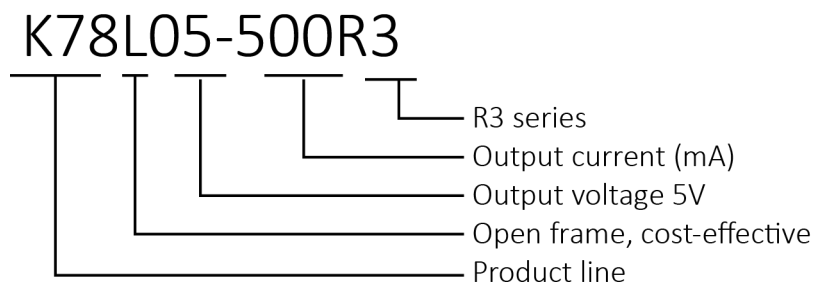


Diagram 1-3 Naming rules of MORNSUN non-isolated switching regulators

## II. Testing Suggestions

It is important that the switching regulators performance is tested and verified in the actual application to ensure that it is suitable. Common test methods include -

### A. Testing the Circuit Itself

Kelvin- style test method is a standard one as shown in diagram 2-1. Test conditions: ambient temperature  $T_a=25^{\circ}\text{C}$ , humidity <75%.

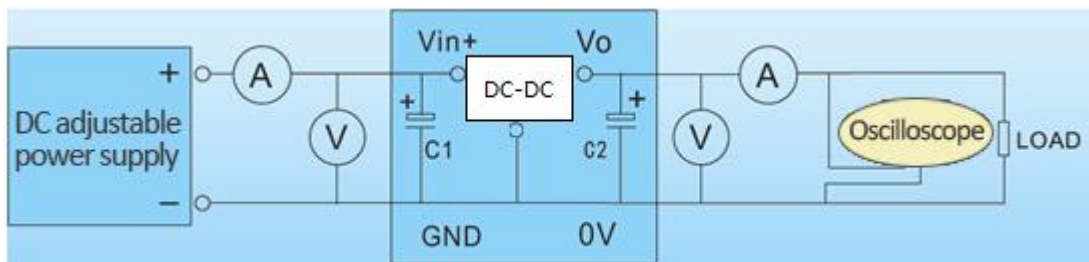


Diagram 2-1 Kelvin-style test method

Test instruments: DC adjustable regulated power supply (wide enough input voltage range), ammeter A (accuracy: 0.001A), voltmeter V (accuracy: 0.001V), electronic load, oscilloscope.

Notes:

a) Wire connection: the less wire loss, the better. A multi-strand copper wire with 1mm diameter is the best choice to avoid excessive voltage drop. When the load current is large shorten the distance between the output pins and the load and increase the cross-sectional area of the connecting wire to reduce the excessive voltage drop.

b) It is suggested to test the output by using contact measuring method with a single pole to prevent measurement errors. The contact measuring method helps reduce external interference and the single pole provides a common ground for the input and output. (See “ripple and noise”)

c) To acquire an accurate voltage and ripple measurement the output capacitive should be within specification and the measurement should be may between 10%-100% of rated load.

d) For more details please refer to datasheet.

## B. Testing Switching Regulator's Performance

Prior to testing it is important to ensure that the switching regulator is correctly connected and that the input and load parameters are within specification. This will ensure that test results are a true reflection of the performance of the device.

### a) Output voltage accuracy:

$V_{outnom}$ : output voltage at nominal input voltage and full load	Output voltage accuracy
$V_{out}$ : tested output voltage at nominal input voltage	$= \frac{V_{out} - V_{outnom}}{V_{outnom}} \times 100\%$

e.g. (K7812-500R2):  $V_{outnom}=12V$ , rated load=500mA,  $V_{out}=12.039V$ ,

$$\text{Output voltage accuracy} = \frac{12.039 - 12.000}{12.000} \times 100\% = 0.325\%$$

### b) Line regulation:

$V_{outn}$ : output voltage at nominal input voltage and rated load	Lineregulation
$V_{outh}$ : output voltage at rated load when input voltage at its upper limit	
$V_{outl}$ : output voltage at rated load when input voltage at its lower limit	
$V_{mdev}$ $V_{outh}$ or $V_{outl}$ which is deviated from $V_{outn}$ more	$= \frac{V_{mdev} - V_{outn}}{V_{outnom}} \times 100\%$

e.g. (K7805-500R2): rated load = 500mA,  $V_{outh} = 5.01V$ ,  $V_{outl} = 5.00V$ ,  $V_{outnom} = 5.01V$ ,

$$\text{Line regulation} = \frac{5.00 - 5.01}{5.01} \times 100\% = -0.2\%$$

### c) Load regulation:

$V_{b1}$ : output voltage at nominal input voltage and 10% load	<p>Load regulation</p> $= \frac{V_b - V_{b0}}{V_{b0}} \times 100\%$
$V_{b2}$ : output voltage at nominal input voltage and 100% load	
$V_{b0}$ : output voltage at nominal input voltage and 50% load	
$V_b$ : $V_{b1}$ or $V_{b2}$ which is deviated from $V_{b0}$ more	

e.g. (K7805-500R2): When load is 100%,  $V_{b2} = 5.01V$ . When load is 10%,  $V_{b1} = 5.02V$ .

When load is 50%,  $V_{b0} = 5.02V$ ,

$$\text{Load regulation} = \frac{5.01 - 5.02}{5.02} \times 100\% = -0.2\%$$

#### d) Efficiency:

$V_{in}$ : nominal input voltage	<p>Efficiency</p> $\eta = \frac{I_{out} \times V_{out}}{I_{in} \times V_{in}} \times 100\%$
$I_{out}$ : output current at full load	
$V_{out}$ : output voltage at full load	
$I_{in}$ : input current	

e.g. (K7805-500R2):  $V_{in} = 12V$ ,  $V_{out} = 4.951V$ ,  $I_{in} = 113.7mA$ ,

$$\eta = \frac{500 \times 4.951}{113.7 \times 24} \times 100\% = 90.72\%$$

#### e) Ripple and noise:

Ripple and noise is the periodic and random AC variation superimposed on the DC output, which affects output accuracy and usually is calculated as a peak-to-peak (mVP-P).

First, set oscilloscope bandwidth 20MHz to effectively prevent high-frequency noise.

Second, test with parallel cable measuring method as shown in diagram 2-2.

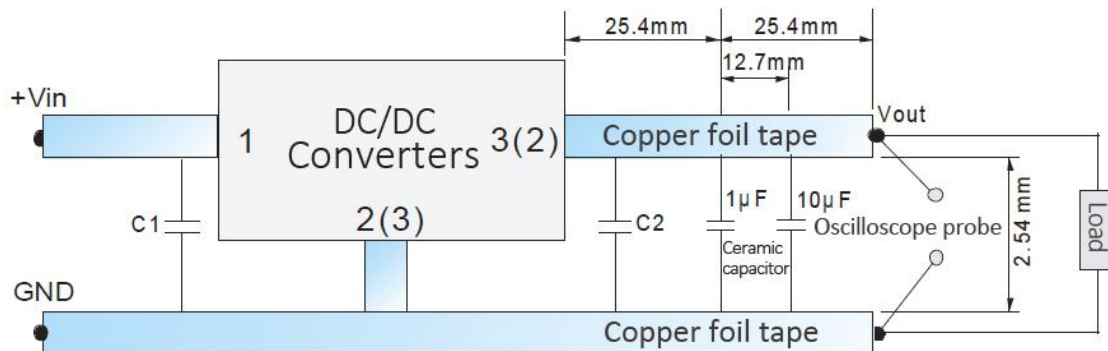


Diagram 2-2 Parallel cable measuring method

Notes:

- C1: a high-frequency ceramic capacitor with 1uF capacitance.
- C2: an electrolytic capacitor with 10uF capacitance and a twice withstand voltage higher than that of the switching regulator.
- Distance between two paralleled copper foils is 2.5 mm and, of which the sum of voltage drops should be less than 2% of nominal output voltage.

The actual tested ripple and noise will vary depending on different circuits and external components. Diagram 2-3 shows the actual tested ripple and noise waveform.

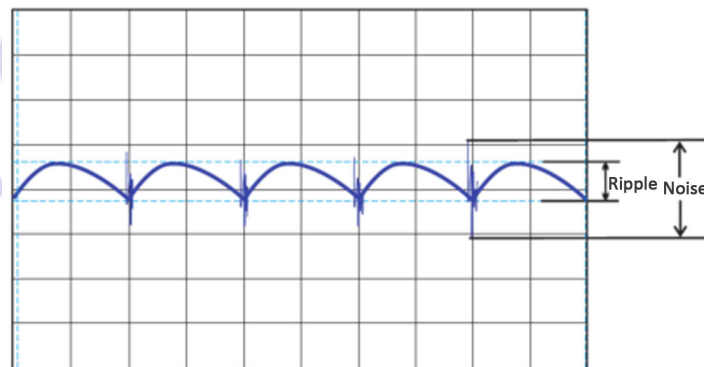


Diagram 2-3 Waveform of Ripple & Noise Test

#### f) Dynamic load:

When the load varies greatly, all the power supplies have a corresponding response time. During this time, the power supply's output voltage will produce instantaneous overshoot and then return to normal state. Dynamic response is an important indicator of switching

regulators performance and is measured by the overshoot and the response time. Common testing method is as shown in Diagram 2-4.

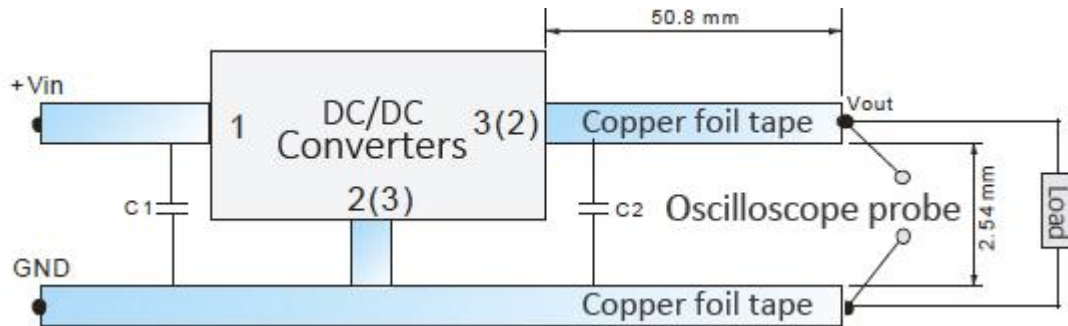


Diagram 2-4 Connection of dynamic load Test

The specific measurement method is to use an electronic load to simulate the sudden change in load. Set the load current at 25% -50% -25% and 50% -75% -50% of the rated load. Next, set the current jumping and falling slope 0.08-0.1A / $\mu$ S. Last, measure the maximum deviation of the output voltage and response time with an oscilloscope. Waveform of dynamic load test is as shown in Diagram 2-5.

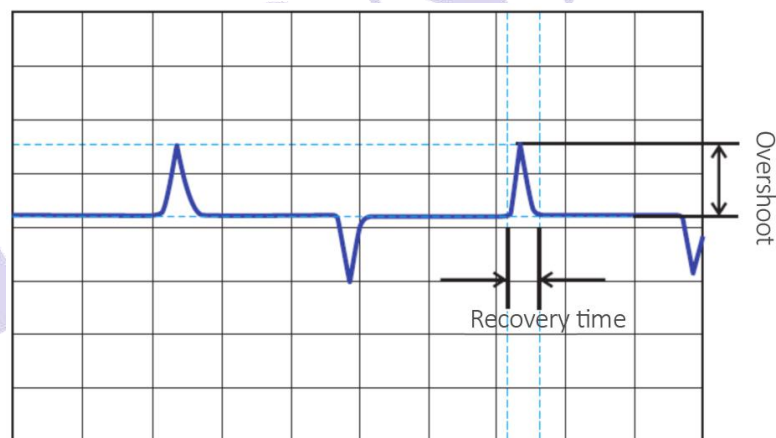


Diagram 2-5 Waveform of dynamic load Test

### g) Start-up time:

Start-up time refers to the delay between the application of the input voltage and the output voltage output voltage reaching its specified output value, this is normally tested at full rated load. In practical design the start-up time and ripple & noise must be considered when designing external filters as this may affect the measured start up delay time.



Diagram 2-6 shows the actual tested start-up time waveform.

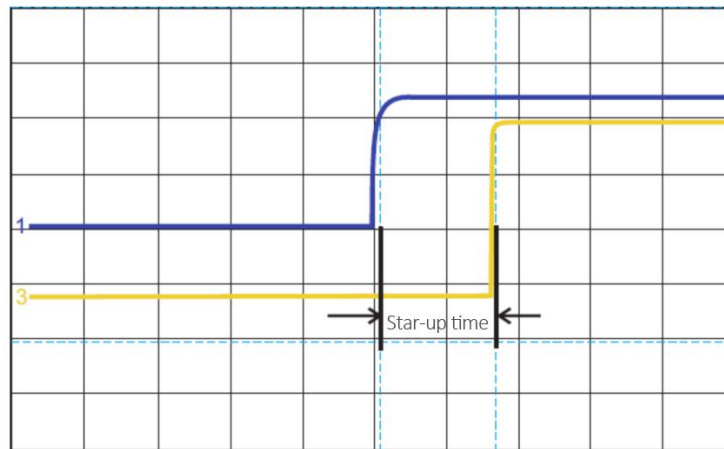


Diagram 2-6 Waveform of Start-up Time Test

#### h) Temperature rise test:

The temperature rise test is usually conducted using a thermal imaging camera or thermocouple. The former may be subject to deviation from the actual value due to emissivity. Testing using a thermocouple is a more accurate measurement method and is therefore recommended.

For example, given that the ambient temperature  $T_a$  is  $25^\circ\text{C}$ , and the measured temperature of power supply  $T_c$  is  $60^\circ\text{C}$ . Then the temperature rise  $\Delta T$  is  $35^\circ\text{C}$  ( $\Delta T = T_c - T_a = 60^\circ\text{C} - 25^\circ\text{C} = 35^\circ\text{C}$ ).

Note: The temperature of the switching regulator will vary due to device power, shell material and internal design, etc. In a confined space, there is no natural ventilation. It is recommended when applying these switching regulators that they are placed away from components that may be sensitive to temperature or isolate them.

### III. Applications of Switching Regulators

#### A. Typical Application

A typical application of K78 series is shown in following Diagram 3-1.

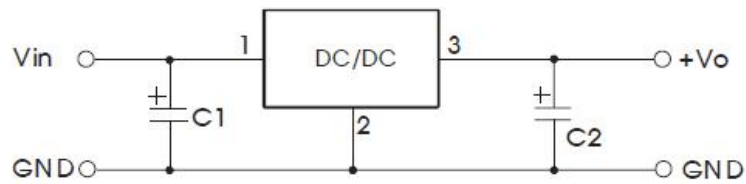


Diagram 3-1 Typical application

The typical output is a BUCK circuit with a recommended external capacitance of 10uF.

### B. Negative Output Application

According to BUCK and BUCKBOOST circuit characteristics, negative voltage output can be achieved by connecting pins 2 and 3, as shown in Diagram 3-2.

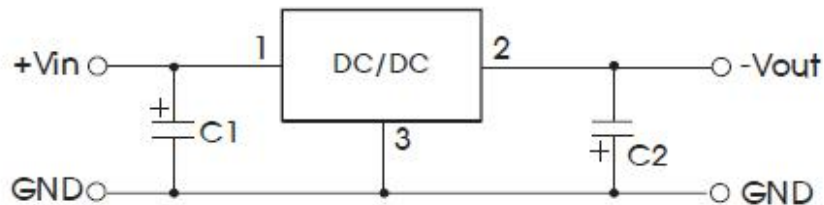


Diagram 3-2 Negative output application

### C. Positive and Negative Outputs Application

To achieve a positive and negative output in the same circuit two switching regulators will be required, as shown in Diagram 3-3.

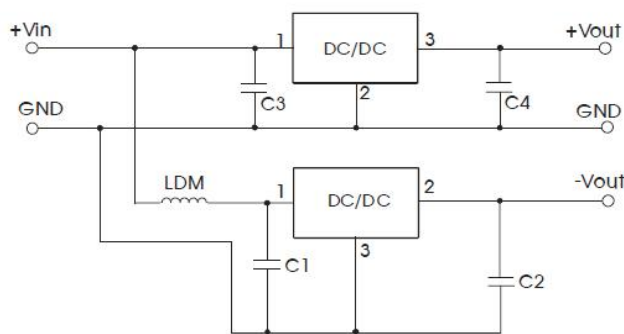


Diagram 3-3 Positive and negative outputs application

It should be noted that start-up current is higher for a negative output configuration as the topology is BUCKBOOST rather than BUCK.

At the same time, in the case of same input voltage, some modules can offer both

positive and negative voltage output while some ones cannot. For example, it's hard to produce  $\pm 15V$  from a same input voltage. The most important reason is that the circuit structure, BUCK or BUCKBOOST, determines switching voltage differences of internal MOSFET in practical application. The MOSFET, however, is difficult to meet the two circuit structure simultaneously. For more detail please refer to the appropriate datasheet.

#### D. Input Reverse Polarity Protection

If there is a possibility that a reverse input may be connected in the application it is recommended that reverse polarity protection is added. The simplest way is to connect a diode in series, as shown in Diagram 3-4.

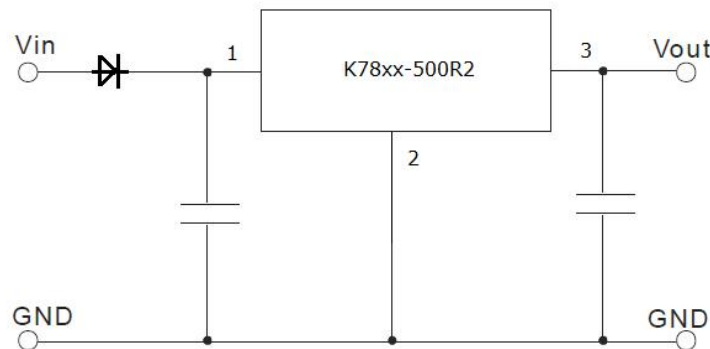


Diagram 3-4 Input reverse polarity protection circuit

In the application it is important to ensure that the diodes voltage drop is taken into consideration with reference to the input voltage requirements of the switching regulator. The diode must also be selected on the basis that its maximum current rating is adequate for the circuit.

#### E. Input and Output Filtering Circuit

Filters are usually connected at the input and output terminals of the converters to reduce ripple and noise in applications which are sensitive. A recommended circuit is as shown in Diagram 3-5.

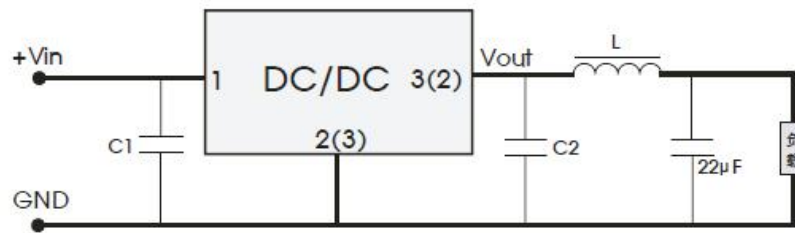


Diagram 3-5 Recommended circuit reducing ripple &amp; noise

C1 and C2 are suggested to refer to datasheet before selecting. Inductance L should be 10uH-47uH.

## F. Electromagnetic Interference and Electromagnetic Compatibility

### a) Electromagnetic Interference (EMI)

EMI is the pollution of the environment by electromagnetic phenomenon through either conducted or radiated means. It cannot be completely eliminated may be reduced to acceptable levels through the application of various filter, layout and shielding techniques. Effective ways to suppress EMI include -

- (1) Shielding EMI radiation: by using converters that have metal packages or by using additional shielding to reduce EMI radiation;
- (2) Grounding techniques
- (3) Selection of suitable filters or filter networks to reduce the transmission of EMI
- (4) PCB layouts that separate switching circuits from small signal circuits to prevent induced noise

### b) Electromagnetic Compatibility (EMC)

EMC is the ability of electronic equipment and power supply to work stably and reliably in environments where electromagnetic interference is present. It is also the ability of electronic equipment and power supply to limit their own electromagnetic interference and avoid interference with other electronic equipment.

Improving EMC is available from the following three aspects -

- (1) Reducing the radiation from sources of EMC interference;
- (2) Shielding EMC interference transmissions

(3) Improve anti-electromagnetic capabilities of circuits.

Transmission of EMC interference is divided into -

1) **Conducted interference.** This is noise generated by the system into the DC input line or signal line. The frequency range of interest is 150KHz-30MHz. Conducted interference is seen as either common or differential mode. An LC network is often used to suppress the conducted interference.

2) **Radiated interference.** This is noise generated as electromagnetic waves, the frequency range of interest is 30MHz-1GHz. Radiation interference can be suppressed by metal shielding.

### c) EMC Solution-recommended Circuit

As DC/DC converters are secondary power supplies, in order to pass EMS test, they usually connect external protection circuit at the DC/DC port or signal port. The protection circuit is as shown in Diagram 3-6.

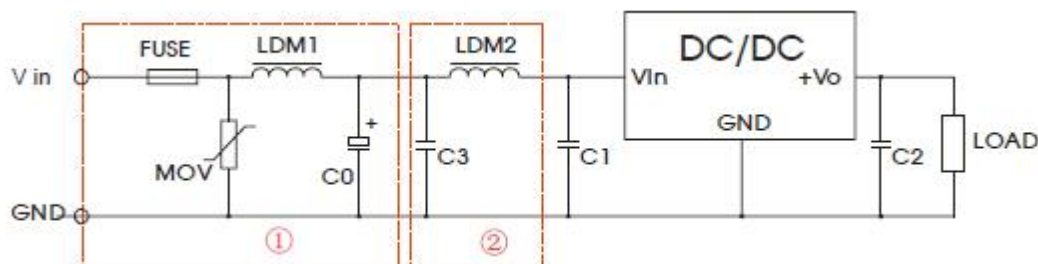


Diagram 3-6 EMC Solution-recommended Circuit

The circuit marked ① is a peripheral circuit for EMS and the circuit marked ② is used for EMI filtering. These circuits can be selected and applied as required and may depend on other circuit elements that may assist or adversely affect the operation on the overall system to EMS and EMI. For more details please refer to the appropriate datasheet.

### G. Capacitive Load

For general switching power supplies, it's recommended to connect electrolytic capacitors at the output terminal to meet the requirements for the maximum capacitive load. But it should be noted that too large a capacitance or low ESR (equivalent series

resistance) may cause the module to work in an unstable mode or may result in start-up issues. For more details please refer to the appropriate datasheet.

## H. Pin-out

### a) TRIM

K78xxT-500 and K78xxT-1000 offer output voltage trimming function. External resistor connection method is as shown in Diagram 3-7.

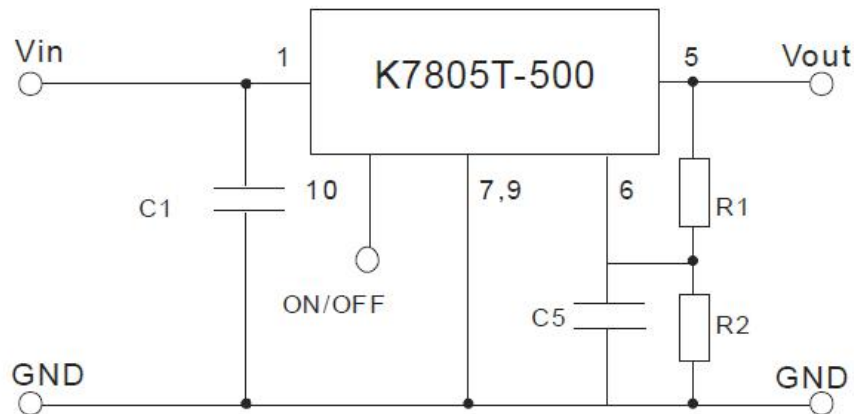


Diagram 3-7 Connection of output voltage trimming with an external resistor

To adjust to a higher output voltage, increase the value of R1 and decrease the value of R2. To adjust to a lower output voltage the inverse applies. If the TRIM is not required the associated pins should be left disconnected.

### b) Switch control

K78xxT-500 and K78xxT-1000 offer switch control function. Switch control refers to the module's output voltage operation of "ON" (enabled) and "OFF" (disabled), as pin 10 shown in Diagram 3-7.

When the voltage  $V_c$  of control pin is between 1.2 and 6V or when there is no connection, the module normally works. When  $V_c$  is at low level (0-0.4V), the module powers off.

## IV. FAQs

### A. Do MORNSUN's switching regulators support hot-plug?

"Hot-plug", simply refers to the plugging or unplugging of converters into the system while the circuit is live.

The switching regulators **MUST NOT** be used in this way as it may result in excessive current flow, voltage spikes or internal damage to the converter.

### B. Can MORNSUN's switching regulators be used at no-load or light-load?

The switching regulators can be used at no-load or light-load applications unless specified. Under such conditions, the conversion efficiency of the converters is relatively low and the converter's control loop may be unstable and produce oscillation. Also, certain parameters may not meet the requirements of datasheet. From the view of reliability it is recommended that the minimum output current is 10%. For best operation it is recommended that the switching regulator is used in a load range of 30-80% of maximum load.

### C. Reasons cause failures of MORNSUN's switching regulators?

Reason 1: Exceeding the maximum capacitive load value stated in the datasheet. Capacitive loads outside of specification may require a larger starting current, this may cause failure of the converters. That reducing the output capacitance at the output terminal or connecting buffer circuit are good choices to increase the capacity of the converters.

Reason 2: The input power supply is not capable of providing the initial start-up current of the switching regulator circuit, this may have a large instantaneous current requirement. In such circumstances it is recommended that a small resistance or NTC is added to the circuit at the input terminal of the switching regulator to reduce the start-up current.

Reason 3: When driving an inductive load (usually motor coil) the circuit resistance seen is very low, usually  $m\Omega \sim \Omega$  level. According to  $I = \frac{V}{r}$ , the output current required

will be in excess of the over the over-current protection value of the converter and as a result the converter will protect the output. To overcome this issue it is recommended that a small resistor is added in series with the output to present a load that will ensure the over-current protection is not triggered, alternatively a switching regulator with a larger output current capability may be selected.

Reason 4: The input voltage is lower than the product's operating voltage, resulting in unstable output.

#### **D. Reasons damaging MORNSUN's switching regulators?**

Five things that may result in damage to the switching regulators, written in *Wide Input Non-Isolated Regulated Output Series Product*.

Reason 1: reverse polarity connection.

Reason 2: the input voltage is much higher than the maximal input voltage, refer to the appropriate datasheet for confirmation on this.

Reason 3: hot-plug produces a larger voltage spike, or input power produces overshoot.

Reason 4: Extreme overload.

Reason 5: The GND is not connected securely, when under heavy load.